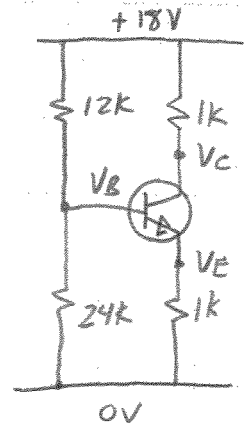


PROBLEM #1a.

Q1 Note: in each case you can start by assuming any of the modes, if you get a self-consistent solution you can stop. All cases are shown here.



(a) Assume cutoff. Then $I_C = I_E = I_B = 0$.

$$\text{Then } V_C = 18 - (0)(1k) = 18V$$

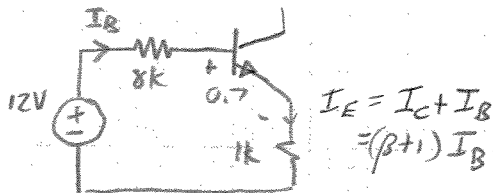
$$V_E = 0(1k) = 0V$$

$$V_B = \frac{24k}{24k + 12k} 18V = 12V$$

But $V_B > V_E$ means forward biased base-emitter. \Rightarrow Not cutoff.

(b) Assume active. Then $V_{BE} = 0.7V$, and $I_C = \beta I_B$.
Reduce left-half of circuit to Thevenin equivalent.

$$V_{oc} = \frac{24k}{24k + 12k} 18V = 12V \quad R_{TH} = 12k // 24k = 8k$$



Loop analysis

$$-12 + 8k I_B + 0.7 + (101) I_B (1k) = 0$$

$$I_B = 103.7 \mu A$$

$$\text{Then } I_C = \beta I_B = (100)(103.7 \mu A) = 10.37 \text{ mA}$$

$$I_E = I_C + I_B = 10.47 \text{ mA}$$

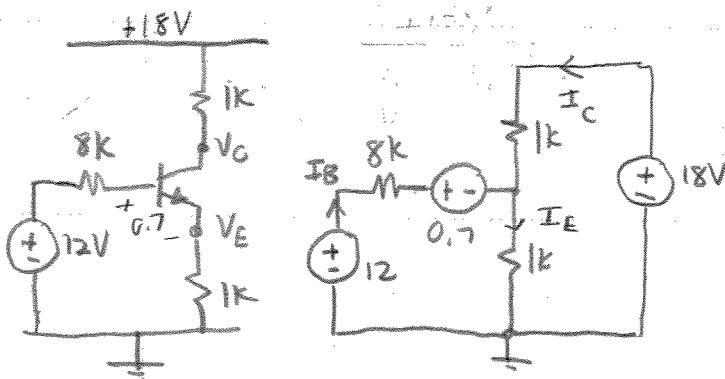
$$V_C = 18 - (10.37 \text{ mA})(1k) = 7.63 \text{ V}$$

$$V_E = (10.47 \text{ mA})(1k) = 10.47 \text{ V}$$

$$V_B = V_E + 0.7 = 11.17 \text{ V}$$

But $V_B > V_C$ means forward-biased collector-base \Rightarrow Not active

(c) Assume saturation. $V_{BE} = 0.7$, $V_{CE} = 0.7 \Rightarrow V_C = V_E$



Left loop

$$-12 + 8k(I_B) + 0.7 + 1k(I_E) = 0$$

$$-12 + 8k(I_B) + 0.7 + 1k(I_B + I_C) = 0$$

Right loop

$$-18 + 1k(I_C) + 1k(I_E) = 0$$

$$-18 + 1k(I_C) + 1k(I_C + I_B) = 0$$

PROBLEM #1a continued.

Simplify: left loop $9kI_B + 1kI_C = 11.3$ } $I_B = 0.271 \text{ mA}$
 right loop $1kI_B + 2kI_C = 18$ } $I_C = 8.865 \text{ mA}$

Then $I_E = I_B + I_C = 9.136 \text{ mA}$

$V_C = 18 - (8.865 \text{ mA})(1k) = 9.135 \text{ V}$

$V_E = (9.136 \text{ mA})(1k) = 9.136 \text{ V}$

$V_B = V_E + 0.7 = 9.836 \text{ V}$

} same rounding error

$V_C = V_E$
 $V_B > V_C$
 $V_B > V_E$

} OK for saturation

$V_E = 9.136 \text{ V}$	$I_E = 9.136 \text{ mA}$
$V_B = 9.836 \text{ V}$	$I_B = 0.271 \text{ mA}$
$V_C = 9.136 \text{ V}$	$I_C = 8.865 \text{ mA}$

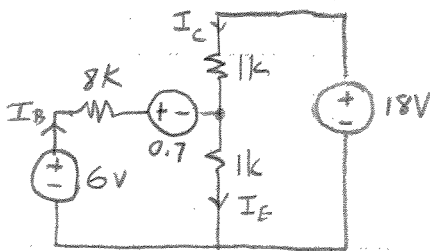
Q2 (a) Assume cutoff

$I_C = I_E = I_B = 0 \Rightarrow V_C = 18 \text{ V}, V_E = 0 \text{ V}, V_B = \frac{12k}{12k+24k} 18 \text{ V} = 6 \text{ V}.$

but then $V_B > V_E$, which means not cutoff

(b) Assume saturation. $V_{BE} = 0.7, V_{CE} = 0.7, V_C = V_E.$

$V_{oc} = \frac{12k}{12k+24k} 18 \text{ V} = 6 \text{ V}, R_{TH} = 12k \parallel 24k = 8k.$



Left loop: $-6 + 8kI_B + 0.7 + 1k(I_E) = 0$
 $-6 + 8kI_B + 0.7 + 1k(I_B + I_C) = 0$
 $9kI_B + 1kI_C = 5.3$

Right loop: $-18 + 1kI_C + 1kI_E = 0$
 $-18 + 1kI_C + 1k(I_B + I_C) = 0$
 $1kI_B + 2kI_C = 18$

Solve: $9kI_B + 1kI_C = 5.3$ } $I_B = -0.435 \text{ mA}$ ← problem already $I_B < 0.$
 $1kI_B + 2kI_C = 18$ } $I_C = 9.218 \text{ mA}$

Current can't flow backward (unless breakdown) through BE junction.

Not saturation.

(c) Assume active. $V_{BE} = 0.7, I_C = \beta I_B.$

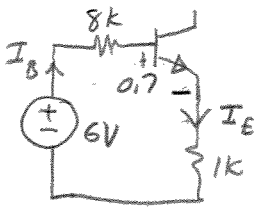
$-6 + 8kI_B + 0.7 + 1k(I_E) = 0$

$-6 + 8kI_B + 0.7 + 1k(\beta+1)(I_B) = 0.$

$I_B = 48.62 \mu\text{A}$

then $I_C = \beta I_B = 4.862 \text{ mA}$

$I_E = 4.911 \text{ mA}$



PROBLEM #1a. Continued.

Then $V_C = 18 - (4.862\text{m})(1\text{K}) = 13.138\text{V}$
 $V_E = (4.911\text{m})(1\text{K}) = 4.911\text{V}$
 $V_B = V_E + 0.7 = 5.611\text{V}$

$V_C > V_B$
 $V_B > V_E$ } = OK for active.

$V_E = 4.911\text{V}$	$I_E = 4.911\text{mA}$
$V_B = 5.611\text{V}$	$I_B = 48.62\mu\text{A}$
$V_C = 13.138\text{V}$	$I_C = 4.862\text{mA}$

Q3 (a) Assume cutoff. $I_E = I_C = I_B = 0$.
 Then $V_E = 12$, $V_C = 0$, $V_B = 0$. But $V_E > V_B$ which is forward-bias for PNP transistor.

Not cutoff

(b) Assume active. $V_{EB} = 0.7$, $I_C = \beta I_B$.
 Then $V_E = 12$, $V_B = V_E - 0.7 = 11.3$. $I_B = 11.3/24\text{K} = 470.8\mu\text{A}$
 $I_C = \beta I_B = 47.08\text{mA}$. $\rightarrow V_C = (47.08\text{m})(1\text{K}) = 47.08\text{V}$.
 47.08V is not possible, also $V_C > V_B$ is forward bias collector-emitter.

Not active.

(c) Assume saturation $V_{EB} = 0.7$, $V_C = V_E$.
 $V_C = V_E = 12\text{V}$. $V_B = V_E - 0.7 = 11.3$. $I_B = 11.3/24\text{K} = 470.8\mu\text{A}$.
 $I_C = 12/2\text{K} = 6\text{mA}$. $I_E = I_C + I_B = 6.471\text{mA}$
 $V_E > V_B$ and $V_C = V_E$. OK for saturation.

$V_E = 12\text{V}$	$I_E = 6.471\text{mA}$
$V_B = 11.3\text{V}$	$I_B = 470.8\mu\text{A}$
$V_C = 12\text{V}$	$I_C = 6\text{mA}$

Q4 (a) Assume cutoff. $I_E = I_C = I_B = 0$.
 Then $V_E = 12$, $V_C = 0$, $V_B = 0$. But $V_E > V_B$, forward-bias for PNP.

Not cutoff.

(b) Assume saturation. $V_{EB} = 0.7$, $V_C = V_E$. Need $I_C < \beta I_B$.
 Then $V_C = 12$, $V_B = 12 - 0.7 = 11.3$. $I_B = 11.3/24\text{K} = 470.8\mu\text{A}$
 $V_C = 12\text{V}$, $I_C = 12/150 = 80\text{mA}$. But then $I_C > \beta I_B$, not possible.

Not saturation.

PROBLEM #1a. continued

(c) Assume active. $V_{EB} = 0.7$, $I_C = \beta I_B$.

$$V_E = 12, V_B = 12 - 0.7 = 11.3, I_B = 11.3 / 24k = 470.8 \mu A$$

$$I_C = \beta I_B = 47.08 \text{ mA}, I_E = I_B + I_C = 47.55 \text{ mA}$$

$$V_C = I_C (150) = 7.062 \text{ V}, V_E > V_B, V_B > V_C. \text{ OK.}$$

$V_E = 12 \text{ V}$	$I_E = 47.55 \text{ mA}$
$V_B = 11.3 \text{ V}$	$I_B = 470.8 \mu A$
$V_C = 7.062 \text{ V}$	$I_C = 47.08 \text{ mA}$

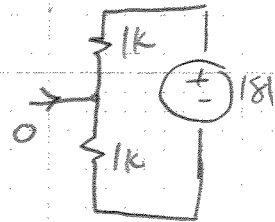
PROBLEM #1b

Repeat all using high- β approximation. Use known correct modes from previous part.

Q1. Saturation: analysis is the same as previous part.

If you ignore I_B , then $V_C = V_E = 9 \text{ V}$, close.

However, this is not safe analysis because you don't know I_B is small.



Q2 Active. Find $V_B \approx V_{OC} = \frac{12k}{12k + 24k} 18 = 6 \text{ V}$

$$\text{Then } V_E = 6 - 0.7 = 5.3 \text{ V}, I_E = 5.3 / 1k = 5.3 \text{ mA}, I_C \approx I_E = 5.3 \text{ mA}$$

$$I_B = I_C / \beta = 53 \mu A, V_C = 18 - (5.3)(1k) = 12.7 \text{ V}, V_E = (5.3)(1k) = 5.3 \text{ V}$$

$$V_B = V_E + 0.7 = 6.0 \text{ V}$$

$V_E = 5.3 \text{ V}$	$I_E = 5.3 \text{ mA}$
$V_B = 6.0 \text{ V}$	$I_B = 53 \mu A$
$V_C = 12.7 \text{ V}$	$I_C = 5.3 \text{ mA}$

Q3 Saturation: analysis is the same as previous part.

Q4 Active: $V_E = 12, V_B = 12 - 0.7 = 11.3, I_B = 11.3 / 24 = 470.8 \mu A$

$$I_C = \beta I_B = 47 \text{ mA}, I_E \approx I_C = 47 \text{ mA}, V_C = (47 \text{ mA})(150) = 7.05 \text{ V}$$

$V_E = 12 \text{ V}$	$I_E = 47 \text{ mA}$
$V_B = 11.3 \text{ V}$	$I_B = 471 \mu A$
$V_C = 7.05 \text{ V}$	$I_C = 47 \text{ mA}$

PROBLEM #3

Q1 Current is flowing, so it is not cutoff.

Guess saturation. $\frac{V_G - (-12)}{560k} + \frac{V_G - 12}{430k} = 0 \Rightarrow V_G = 1.576 \text{ Volts}$

$I_S = 25 \text{ mA}$, $I_D = I_S = 25 \text{ mA}$, $V_D = 12 - (25 \text{ mA})(150) = 8.25 \text{ Volts}$.

Use $I_D = \frac{1}{2} k_n' \left(\frac{W}{L}\right) (V_{GS} - V_t)^2 \rightarrow 25 \text{ mA} = (4 \text{ mA})(V_{GS} - 1)^2$

solve: $V_{GS} = \begin{cases} -1.5 \leftarrow \text{cutoff, } V_{GS} < V_t \\ \textcircled{3} \leftarrow \text{pick this one} \end{cases}$

$V_S = V_G - V_{GS} = 1.576 - 3.5 = -1.924 \text{ Volts}$

Check $V_{GS} > V_t$, OK $V_{DS} > V_{GS} - V_t \rightarrow V_D > V_G - V_t$, OK

$I_D = 25 \text{ mA}$, $V_D = 8.25 \text{ Volts}$, $V_G = 1.576 \text{ Volts}$, $V_S = -1.924 \text{ Volts}$

Q2 Guess saturation. $\frac{V_G - (-12)}{220k} + \frac{V_G - 12}{680k} = 0 \Rightarrow V_G = -6.133 \text{ Volts}$

$I_D = \frac{1}{2} k_n' \left(\frac{W}{L}\right) (V_{GS} - V_t)^2$, also $I_D = I_S = \frac{V_S - (-12)}{180}$

$\frac{V_S + 12}{180} = (4 \text{ mA})(-6.133 - V_S - 1)^2$

simplify $0.72V_S^2 + 9.272V_S + 24.633 = 0 \Rightarrow V_S = -6.439 \pm 2.692$

$V_S = \begin{cases} \textcircled{-9.131} \leftarrow \text{pick this one} \\ -3.747 \leftarrow V_G < V_S \text{ cutoff} \end{cases}$

$I_S = \frac{-9.131 - (-12)}{180} = 15.94 \text{ mA} = I_D$, $V_D = 12 - (250)(15.94 \text{ mA}) = 8.02 \text{ Volts}$

Check $V_{GS} > V_t$, OK, $V_{DS} > V_{GS} - V_t$, OK

$I_D = 15.94 \text{ mA}$, $V_D = 8.02 \text{ V}$, $V_G = -6.133 \text{ V}$, $V_S = -9.131 \text{ V}$

Q3 Guess saturation. $\frac{V_G - (-12)}{680k} + \frac{V_G - 12}{220k} = 0 \Rightarrow V_G = +6.133 \text{ Volts}$

$I_D = \frac{1}{2} k_n' \left(\frac{W}{L}\right) (V_{GS} - V_t)^2$, also $I_D = I_S = \frac{V_S - (-12)}{250}$

$\frac{V_S + 12}{250} = (4 \text{ mA})(6.133 - V_S - 1)^2$

simplify $V_S^2 - 11.266V_S + 14.347 = 0 \Rightarrow V_S = 5.633 \pm 8.339$

$V_S = \begin{cases} 13.972 \leftarrow \text{not possible, } > 12 \text{ V power supply.} \\ -2.704 \leftarrow \text{pick this one.} \end{cases}$

PROBLEM #3 continued.

$$I_D = \frac{V_S - (-12)}{250} = \frac{-2.704 + 12}{250} = 37.18 \text{ mA}$$

$$V_D = 12 - (37.18 \text{ m})(250) = 2.704 \text{ Volts.}$$

check $V_{GS} > V_t$, OK, check $V_{DS} > V_{GS} - V_t$, not OK. V_{DS} is $< V_{GS}$.

Guess again: triode. $V_G = +6.133$ Volts, same as above.

$$I_D = k_n' \left(\frac{W}{L} \right) \left[(V_{GS} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 \right]^2$$

$$\text{also } I_D = I_S = \frac{V_S - (-12)}{250} \Rightarrow V_S = -12 + 250 I_D$$

$$I_D = \frac{12 - V_D}{180} \Rightarrow V_D = 12 - 180 I_D$$

$$\begin{aligned} I_D &= (8 \text{ m}) \left[(6.133 - V_S)(V_D - V_S) - \frac{1}{2} (V_D - V_S)^2 \right] \\ &= (8 \text{ m}) \left[(6.133 + 12 - 250 I_D)(12 - 180 I_D + 12 - 250 I_D) \right. \\ &\quad \left. - \frac{1}{2} (12 - 180 I_D + 12 - 250 I_D)^2 \right] \end{aligned}$$

Simplify

$$120.4 I_D^2 - 27.818 I_D + 7.1776 = 0 \quad I_D = 0.1155 \pm 0.0597$$

$$I_D = \begin{cases} \underline{0.0558} & \leftarrow \text{pick this one} \\ 0.1752 & \leftarrow V_S \text{ is too high if you use this} \end{cases}$$

$$V_S = -12 + (0.0558)(250) = 1.95 \text{ V}$$

$$V_D = 12 - (0.0558)(180) = 1.956 \text{ V}$$

check $V_{GS} > V_t$, OK $V_{DS} < V_{GS} - V_t$, OK

$$\boxed{I_D = 55.8 \text{ mA}, V_D = 1.956 \text{ V}, V_G = 6.133 \text{ V}, V_S = 1.95 \text{ V}}$$

Q4 Guess saturation. $V_D = V_G$. $I_D = \frac{12 - V_D}{1.5 \text{ K}}$. $V_S = -12$.

$$I_D = \frac{1}{2} k_n' \left(\frac{W}{L} \right) (V_{GS} - V_t)^2 \Rightarrow \frac{12 - V_D}{1.5 \text{ K}} = (4 \text{ m}) (V_D - (-12) - 1)^2$$

$$\text{Simplify } 6V_D^2 + 133V_D + 714 = 0 \Rightarrow V_D = -11.0833 \pm 1.9597$$

$$V_D = V_G = \begin{cases} -13.043 & \leftarrow \text{not possible, less than } -12 \text{ V} \\ \underline{-9.124} & \leftarrow \text{pick this one} \end{cases}$$

$$I_D = \frac{12 - (-9.124)}{1.5 \text{ K}} = 14.08 \text{ mA. } V_{GS} > V_t, \text{ OK } \quad V_{DS} > V_{GS} - V_t, \text{ OK }$$

$$\boxed{I_D = 14.08 \text{ mA}, V_D = -9.124 \text{ V}, V_G = -9.124 \text{ V}, V_S = -12 \text{ V}}$$